

PILIKO, V.M.

Chlorosis in plants due to iron and manganese deficiency in soils. Bot. zhur. 45 nc.8:1232-1235 Ag 60.
(MIRA 13:8)

1. Astrakhanskaya gosudarstvennaya oblastnaya sel'skokhozyaystvonnaya opytnaya stantsiya, g. Astrakhan'. (Chlorosis (Plants)) (Plants, Effect of iron on) (Plants, Effect of manganese on)

PIL'KO, Vledimir Natveyevich; BULGAKOV, L.P., kand.sel'skokhoz.nauk, otv. red.; TOHKAYLO, I., red.; KALECHITS, G., tekhn.red.

[Pertility of the soils of White Russia] Plodorodie pochv BSSR.

Minsk, Gos.izd-vo BSSR, Red.sel'khoz.lit-ry, 1959. 195 p.

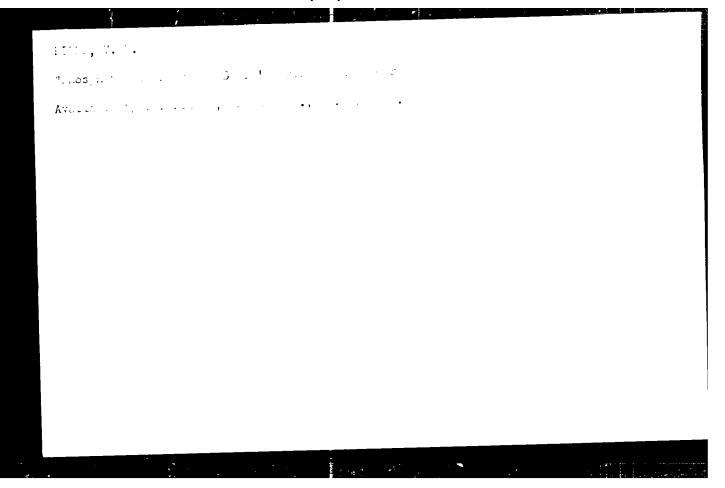
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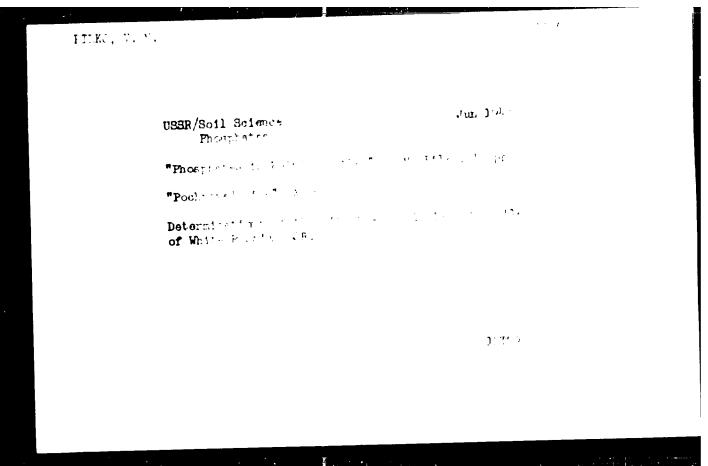
(White Russia--Soils)

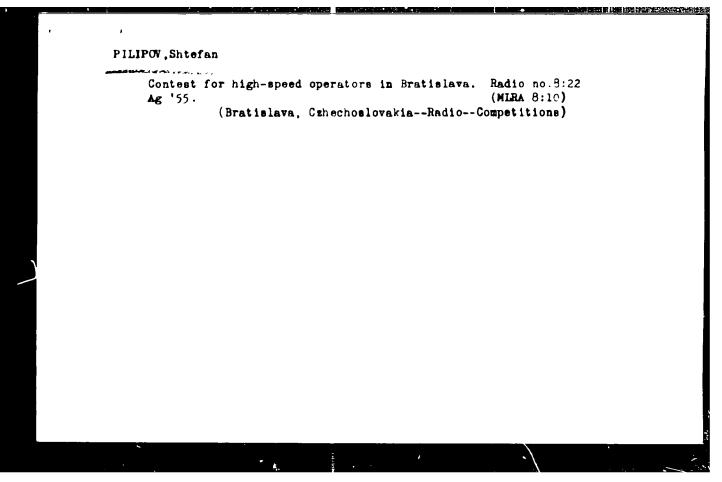
PIL'KO, V.M., kand.sel'skokhozymystvennykh muk

Soil surveys in Vileyka District. Zerleielie ? nc.l:ALAL
Ja '59.

(Vileyka District-Soil surveys)







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PHILS, L.

PHILS, L. Use of metallic calcium; an excerpt from an article. p. 13.

Peaceful use of thermonucleur energy. p. 1h.

The antiprotor. p. 18.

Use of light metals in the mulcin industry. p. 19.

The Exhibition of Mining in Paris. p. 22.

Experimental dwellings made of prefabricated panels. p. 29.

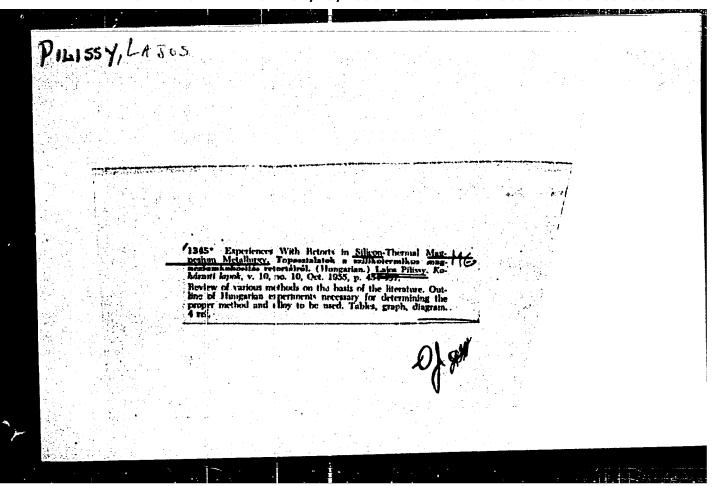
Genesis of electrostatic charge in the textile industry. p. 27.

Vol. 11. No. 12, June 1956.

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TECHNOLOTY

Budapest, Hungary

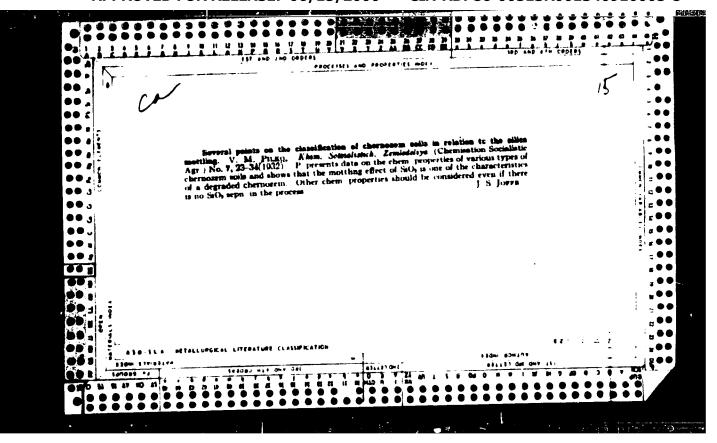
So: Last European Accession, Vol. 7, No. 2, Teb. 1957

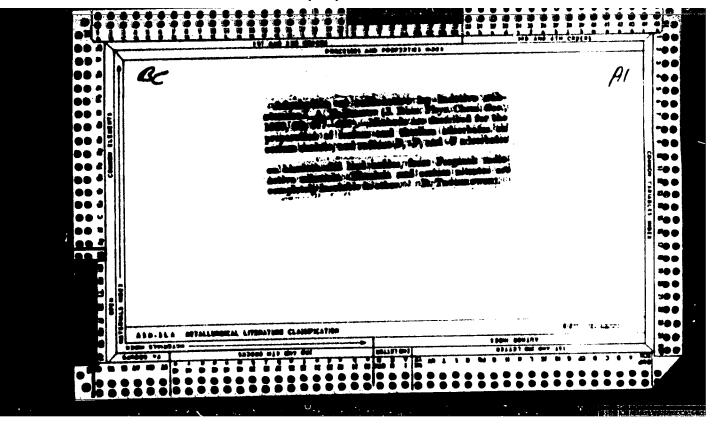


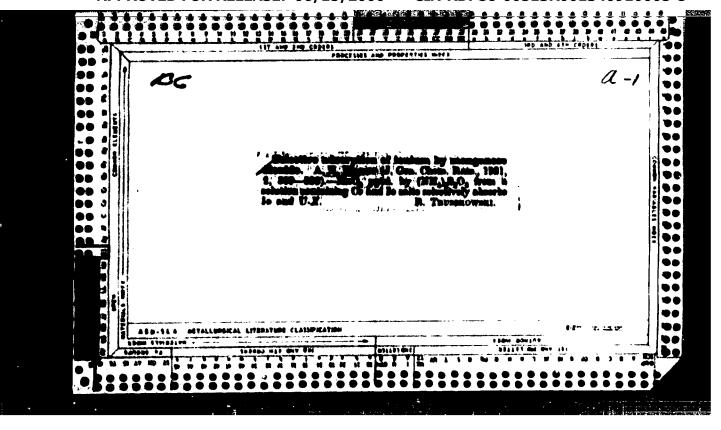
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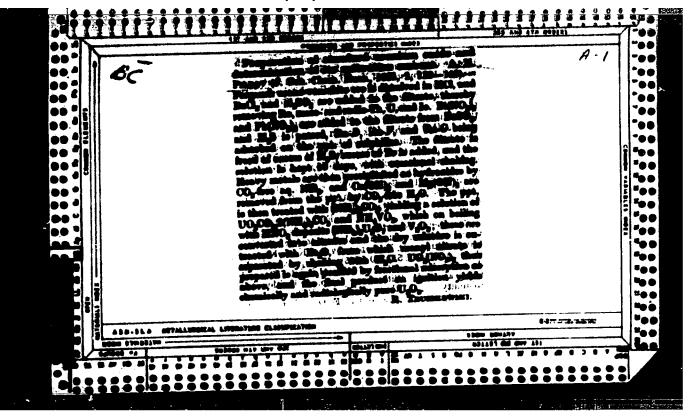
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Abstractor's note: The translation

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8/137/62/000/001/095/237 A052/A101

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Pilous Vaciav

TITLE:

- AUTHOR:

Welding bast steel with 13% Cr [4CH 422905 (ChSN422905)]

PERIODICAL:

Referativnyy zhurnal. Metallurgiya, no. 1, 1962, 12, abstract 1E65 (Zvaranie, 10, no. 7, 1961, 198 - 202; Slovakian; summary in

English, Russian, German)

TEXT: It is pointed out that stainless steel with 13% Cr is brittle and hard and unsuitable for welding. In accordance with the technology of production, castings after naving been taken out of the mold are subjected to soft annealing at $70G - 75C^{\circ}C$ with a slow cooling-down. In this state their hardness and $C_{\rm K}$ are low. Castings repaired by welding must undergo heat treatment prior to welding (hardening at $950-1,000^{\circ}C$ with air cooling and tempering at $700-750^{\circ}C$). After heat treatment the surface of castings is ground, magnetic control and handling of defects before welding are done. The welding is performed with E384 or 13% Cr-Ni electrodes. Prior to welding the castings are

Card 1/2

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Welding cast steel	8/137/62/000/001 / 095/2 A052/A101
preheated to $250 - 400^{90}$. The final heat nealing at $950 - 1,050^{90}$, hardening at 900 .	treatment consists of diffusion an- -950°C and tempering at 700-720°C.
	V Tarisova
[Abstractor's note: Complete translation]	
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Card 2/2	

2/046/62/000/001/007/007 D007/D102

12200

AUTHORS:

Koutsky, J., Lagineer, Candidate of Sciences, and Pilous, V.,

lingineer, Candidate of Sciences

TITLE:

welding modified 12% chromium steels used at the Lenin Works in

Plach

PERIODICAL:

Zváračský sborník, ro. 1, 1962, 154-169

The Lemmony ravidy (Lemmonks) in Plzen, in co-operation with tenelektrodovna VIKO (Llectrode Plant, VIKO) in Ostrava and the IAI in Zamberk, developed the L 55 electrode for welding T 58 and T 59 steels which are used by the Lemin works for production of pover equipment designed for service at temporatures up to 60000. The weld metal of the L 55 electrode has a chemical composition similar to the T 55 steel (approximately 0.16 % 0; 11% or; 1% Ni; 2% W; 0.3% V) and is of martensitic structure with a ferrite-delta content up to 5%. Its mechanical values at 2000, and the creep-strength values at 60000 after heat treatment are relatively high and satisfactory for both T 58 and T 59 parent metals. Helding is done with preheating to 350-40000. Before heat treatment, the welded

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z/c46/62/000/001/007/007 D007/D102

Welding modified 12% chromium steels ...

joint has to be cooled below 100°C, then a full heat treatment, and eventually refining, is performed. For extreme cases tempering at 730°C for 5 hours with cooling in air is recommended. The notch-toughness values of the weld-parent metal transition correspond to those of the T 58 and T 59 parent metals. There are 20 figures, and 4 tables. (Technical editor: Doctor of Natural sciences A. Zapletálek, VUZ Bratislava)

ASSOCIATION: Leninovy zavody (Lerin works), Plzen

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KOUTSKY, J., doc., inz., C.Sc.; PILOUS, V., inz., C.Sc.

Conference of the humanian Academy of Sciences in Timisoara. Hut
listy 18 no.3;224-226 Mr '63.

1. Zavody V.I. Lenina, Plzen.

z/034/63/000/003/004/004 B073/B335

Koutský, L., Doctor Engineer, Candidate of Sciences, AUTHORS:

and Pilous, V., Engineer, Candidate of Sciences

Conference of the Rumanian Academy of Sciences in TITLE:

Timisoara

Hutnické listy, no. 3, 1963, 224 - 226

A conference on the welding and testing of metals, PERIODICAL: convened by the Technical Section of the Rumanian Academy of TEXT: Sciences, was held in Timisoarabetween October 12 and 15, 1962. The following papers were read: Academician Miclosi: selection of steels for welded structures; Professor Doctor St. Nadasan: present state of testing steels; Academician K.K. Khrenov: new current sources for electric-arc welding; Engineer Ion Avram: methods and equipment for welding pressure vessels and pipes made of carbon and alloy steels (review of three papers submitted by individual authors); Professor Engineer Dan Hateoscu: welded building and machine structures (review of four papers submitted by individual authors); Engineer Josif Hajdu: static and dynamic tests (review of six papers submitted by individual authors); Card 1/3

Z/034/63/000/003/004/004 E073/E335

Conference of

Engineer Viorel Miclosi: pressure-welding and additives (review of three papers submitted by individual authors); Engineer Ovidiu Centea: flame-and electric-arc-cutting of metals (review of several submitted papers); Engineer M. Ratiu: test methods and test machines (review of four individually submitted papers); Engineer T. Salagean: additive materials (review paper summarizing experience gained in the manufacture of additive wires, electrodes and fluxes in Rumania); Engineer Vl. Popovici: various processes of welding high-grade alloy steels (review of several presented individual papers); Engineer L. Boleantu: non-destructive testing of metals (review of three submitted individual papers, including one on using betatrons for defectoscopy purposes); Engineer A, Ivancenco: new methods of welding (review paper on welding under flux, welding in a protective carbon-dioxide atmosphere and in an argon atmosphere); Engineer A. Bernath: fatigue-testing of metals (review of seven individually submitted papers); Engineer Josif Bonescu: problems of testing welding machines and of work safety (review paper). The conference was attended by over 230 Rumanian and 40 foreign specialists (5 Czech, 7 Polish, 9 East German, 17 Hungarian).

Conference of Z/034/63/000/003/004/004 E073/E335	•
The authors consider the contribution of Academician Miclosi on the "selection of steel for welded structures" to be the most interesting.	i .
ASSOCIATION: ŽVIL, Pilsen	
Gard 3/3	

LOBL, Karel, inz., kandidat technickych ved; PILOUS, Vaclav, inz.

Welding thick-walled austenitic castings for the power inquetry. Zvar sbor 10 no.2:169-185 61.

1. Statni vyzkumny ustav materialu a technologie, Praha; Vyzkumny a zkusebni ustav, Lennovy zavody Plzen.

s/123/62/000/012/010/010 A004/A101

AUTHORS:

Koutský, J., Pilous, V., Pokorný, R.

TITLE:

Developing modified steels with 10% Or for steam and gas turbine parts at the Flants im. V. I. Denin at Fizen (Republic of Szechisslovakia)

PERIODICAL: Referativnyy zhurna., Masninostroyenive, no. 12, 1857, 4 - 4, Russian, German and English summaries)

A highly heat-resistant T 56 stee, grade of the martensite type has TFXT: been developed (0.16 - 0.5 C, 1..5 - 12.5% Cr, 2.0 - 2.5% \ 0.15 - 0.15 V, 0.5 - 1.0% Ni), which is used in the manufacture of forged gas turbine parts. Another newly developed heat-resistant T 59 grade steel (0.70 - 0.15% C, 11.5 -13.5% Cr, 0.5 - 0.8% W, 0.10 - 0.20% V, 0.5 - 1.0% Ni) représents a transition grade between the classic steel with 12% Cr and its highly heat-resistant modification, and is suitable for the manufacture of cast parts operating at $500^{\rm Ge}$. After oil-hardening at 1,050°C and tempering at 680°C the T 58 grade steel has

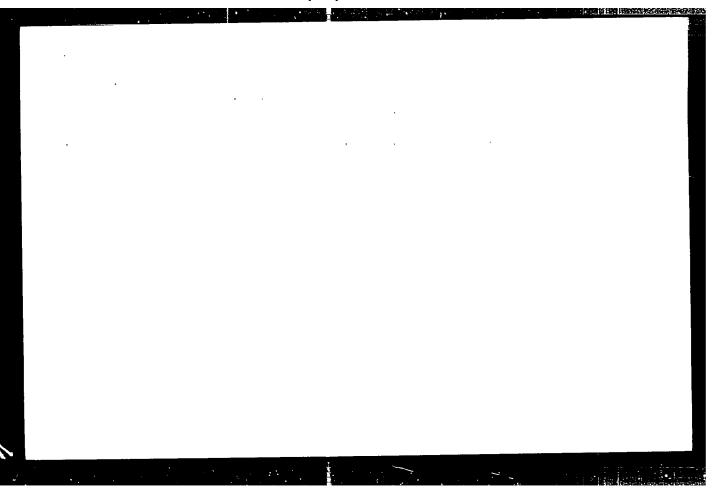
Card 1/2

Developing modified steers with...

S/123/02/000/012/010/01 A004/A101

 $_{\rm D}$ = 80 kg/mm², $_{\rm S}$ = 60 kg/mm², $_{\rm C}$ = 5% and $_{\rm K}$ = 9 kgm/cm². The optimum on 1.tions for the T 59 grade steel are ... (5) $^{\circ}$ C (4 mours) (cooling in air), r = (6 nours) (air) or $^{\circ}$ COC (6 nours) (air); $^{\circ}$ C = $^{\circ}$ C rg/mm², $^{\circ}$ S = 55 rg/mm², $^{\circ}$ E av = 5 - 6 kgm/cm2. The modified steel grades T 58 and T 59 with 175 or on the welded with electrodes having the same meananteal properties as the base material. Such electrodes, which have been specially developed with the brands Fish and E 58M, yield seams without cracks with a creep limit at 600°C which corresponds to the values of the steels to be welled (at 100,000 hours and 600° C not less than 11 kg/mm² for the T 58 grade and 4 kg/mm² for the T 59 grade steel). The E 58 electrodes produced from a steel modified with 2 - 2.5% W and V, yielia seam with $a_{k} = 1.5 - 2.5 \text{ kgm/cm}^2$, this value being 4.0 - 8 kgm/cm² after heat treatment. These electrodes are suitable for weiding material up to 15 mm thi kness, intermediate annealing is required with material of greater thickness. The E 58M electrodes contain 6.4 - 6.0% [Abstracter's note: no designation given] and are suitable for welding material of more than 35 mm thickness in the case of an intermediate annealing being impracticable. The advantage of the E 58M electrode over the E 58 grade is the higher as value of the former, which amounts to 1.8 - 3 kgm/cm2 after welding and 5 - 9 kgm/cm2 after heat treatment. [Abstracter's note: Complete translation]

Card 2/2



CZECH/34-59-5-9/19 Pilous, Vaclay, Inc. AUTHOR:

Weldability of Skoda T-56 High Creep Strength Cr-W-Mo-V steels in the Forged State (Svaritelnost TITLE:

%árupevné oceli Cr-W-Mo-V Škoda T56 v kovaném stavu)

PERIODICAL: Hutnické Listy, 1959, Nr 5, pp 429-435 (Czechoslovakia)

AbSTRACT: This steel (which is patented in several countries) has

been developed by the Research Laboratories of the Skoda Works. It is a ferritic-pearlitic alloy steel and is made with alloying elements relatively easily

available in Czechoslovakia. It is intended for producing castings for steam turbines and in the forged state for rotors of 100 to 200 MW unit rating turbines operating with steam of an initial temperature of 565 C.

It is superior to the Cr-W-V steels TBW-50 and Loc-315 at present used for the same purpose. In the work described in this paper the metallurgical aspects of the weldability of this steel in the forged state were investigated using V Lof Spec Extra Czech produced

(Cr-Mo-V) electrodes. The results can be summarised thus: Card 1/3 1. The steel Skoda T56 is weldable only in the heat

GZECH/34-59-5-9/19

Weldability of Škoda T-56 High Creep Strength Cr-W-Mo-V steels in the Forged State

treated state and if possible it should be effected after tempering at 750°C.

2. Austenite to martensite transformation during welding is prevented by pre-heating the forgings to 380°C for 15 mins. The resulting structure after welding of the weld metal and of the transition zone is bainite which, after tempering at 750°C, becomes transformed into a ferrite-carbide structure.

3. After cooling from 1030°C at a speed of 1000 to 250°C/hr, the base material has low values of impact strength. Therefore, great attention must be paid to the pre-heating temperature during welding. In the case of welding 25 mm plates with pre-heating to 380°C the cooling speed in the transient zone in the temperature range 750 to 600°C is 40 000°C/hr. At higher pre-heating temperatures the cooling speed drops sharply and cracks may occur in the transient zone in the case of welding material of a large thickness. In the case of welding thick rings, where the heat conductivity is low, it is necessary to reduce the V

Weldability of Skoda T-56 High Creep Strength Cr-W-Mo-V Steels in the Forged State

content to a value which applies for cast steel Skoda T56 or to carry out the welding in such a way that the cooling speed in the transient zone does not reach critical values.

4. The Czech electrode material, V. Lof Spec Extra, is suitable for welding this steel. After sustained loading at elevated (operating) temperatures, the transition between the base material and the weld metal is gradual and has a ferrite-carbide structure. There are 13 figures, 7 tables and 10 references, 4 of which are Czech, 3 Soviet, 2 English, 1 German.

ASSOCIATION: Výzkumný a zkušební ústav Závodu V. I. Lenina, Plzeň (Research and Test Institute V. I. Lenin Works, Pilsen)

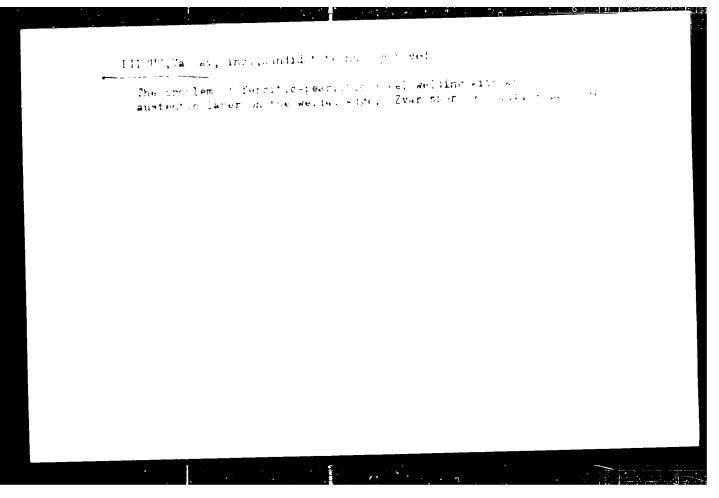
SUBMITTED: February 7, 1959

Card 3/3

PHONS, Vaclav, inz., Sec.

Third International Colloquy on Steel Weldability in Weinar. Zvaranie 12 no. 6: 177-178 Se 165.

1. Leninovy zavody Plzen.



KOUTSKY, J., inz., C.Sc.; PILOUS, V., inz., C.Sc.

Welding of modified 12 per cent Cr steels used in the Lenin Works in Plzen. Zwar sbor 11 no.1:154-169 '62.

1. Leninovy zavody, Plzen.

PILOUS, Vaclav, inz., C.Sc.

New experience with the welding of alloy steel and alloys in Leninovy zavody [Lenin Works] in Plzen. Zvaranie 11 no.5:130-135 My '62.

1. Leninovy zavody, Plzen.

PAWERA, Karel, inz.; PILOUS, Vaclav, inz., kandidat technickych ved; POBOKIL, Frantisek, inz., dr.

Microstructure and mechanical properties of weld joints of austenitic and ferrite pearlitic creep resisting steel for boilers with high parameters. But listy 16 no.3:186-197 Mr. 1/2

- 1. Vitkovicke zelezarny Klementa Gottwalda, Ostrava (for Pawera .
- 2. Zavody V.I.Lenina, Vyzkumny a zkusebni ustav, Plzen (for Pilous).
 - 3. Vyzkumny ustav hutnictvi zeleza, Praha (for Poboril).

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Hilmis, Vaciav

77 mr. p

om the problem of weldirg steels with different structural take

FFFI WIL AL

Peterativnyy zhurnal, Metallorgiya, no. 8, 1961, M., atotra totter ("Tvaranie", 1964, 9, no. 9, % -264, Thechoslovak

Weiding rids of all will B3yr (VDFe) is staining of right of William Fe, and also W. Mo. Ti, and A., were cast in a sand moid (the root length was resonant manifered mome). Thereupon the rods were forged to a diameter of room modes a rodo were used to weld steel 41-21. (ferrite + pearlite) and 41.44. These rodo were used to weld steel 41-21. (ferrite + pearlite) and 41.44. The seam metal at also and 41.67. For the seam metal at also and 41.67. For the seam metal at an also and 41.67. We so and 55% respectively; $a_k \gg c_k m' m$. Due to the fact that the perfect of linear expansion of the metal of the rod VDFe is intermediate to that of the steel weight, better results are obtained by mean. It than by welding with rote if steel 11-7. There are a reference, it is never to put at attaches see EZhMet, 1961, 480.

Aristractor's note: Complete transportion?

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AUTHOR:

Pilous, Václav, Engineer, Candidate of Technical

Sciences

TITLE:

A contribution to the question of ferrite-pearlities

steel welding with an austenitic cushion

PERIODICAL: Zváračský sborník, no. 4, 1960, 439 - 444

TEXT: The article indicates methods for determining the wellatiiity of steel with different structural basis (austenitic and ferropearlitic). The detailed study at VOZ in Bratislava established the advantage of sequence welding during which a "cushion" of a low-carbon electrode (E 44.83) with 0.06 - 0.08 % carbon content is welded onto a low-alloy material. The filling weld is by the austenitic stabilized electrode (E 391). The carbonization of the austenitic weld does not occur due to the low carbon content of electrode E 44.83. This welding procedure was worked out by Amademician I. Cabelka (Ref. 1: SAV Bratislava 1953). The impact

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strength of the toe layers is satisfactory after welling and teat treatment. The weld can be used up to the working temperatures of high-alloy cladding steel if the load bearing steel is not very thick. The arc-welded heat resisting butt-joint with auxiliary material can be used for working temperatures from 450 to 500°C, which there is still no carbonization of austenitic welding metal from the low-alloy material due to the low-carbon "cushion". The contra between austenitic and low-alloy materials for the welding tempe rature in the range 500 - C should be made by 18/8 CrN: e.c. trodes, according to the element. The large decarbonized somes al toe adjacent to the auster. 'I seeoccur in the low alloy made ting metal during heat trootment at working temperatures. The arbonization and decarbonization is due to the different a lat. 1.15 of garbon in alfa and gamma phases as quoted in F.D. E. narra n (nef. 4: Journal of the Iron and Steel Inst. IX. 19.1. 17.1. The yello thermal stress at 500 - 600°C additional to the leafur Stress lauses cracks in a region close to the austenitic well solar This is due to the different thermal expansion posificient of the

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austenitic welding material and the basic ferro-pearlitic material. One solution for preventing cracking is to form an anti-diffusion barrier between these two materials which prevents the transit of carbon from the low-alloy steel to the austenitic welding metal. The Leninovy zavody, Plzeň (Lenin Works in Pilsen) solved the problem by using auxiliary rods VZ having 60/18 NiCr. This welding material has a coefficient of thermal expansion between the low-alloy ferro-pearlitic and the austenitic material coefficients so that cyclic thermal stresses are not so critical and also the solubility of carbon in VZJ welding metal is small. The rods are manufactured by casting instead of rolling which is an advantage compared with foreign rods. Due to the shortage of nickel they are used mainly for welding alloy VZU of the distributors for gas turbines. Otherwise they are used as "cushions" of low-alloy ferro-pearlitic materials while the filling electrode is of type 18/8 CrNi. The welding of VZU layer is made in a protective argon atmosphere to form an effective barrier against carbon diffusion. The filling weld is made by austenitic electrodes 18/8 CrNi (E 391 or E 891).

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The welding is made by pre-heating to a temperature corresponding to the low-alloy material and afterwards the weld is tempered to the temperature of low-alloy material (material 15 225 - tempering the temperature 720°C). The impact strength and hardness established temperature 720°C). The impact strength and hardness established for tempering the weld by the direct weldability test VJS 25 is shown in Fig. 7.

Fig. 7. Results of direct weldability tests VUS 2S.

Legend: 1 - Hardness H_v ; 2 - impact strength in mkg/cm^2 ; 3 - distance from toe in mm; 4 - impact strength; 5 - hardness.

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V3LV E 381 15,225

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A contribution to the ...

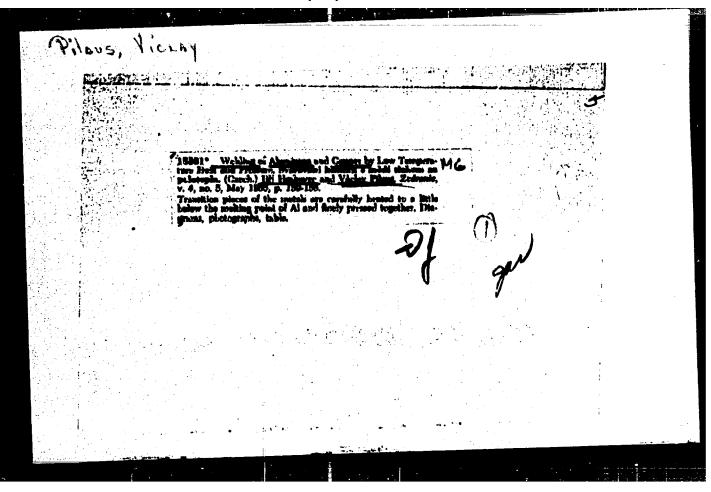
The maximum impact strength is 5.2 mk/cm², the hardness is between 190 - 216 Hy. The maximum hardness is the affected region was obtained after olding close to the too edge - 320 Hy. The samples were left at 0° C during loading 15 kg/mm² after heat treatment. After 1500 is there was no breaking of the test pieces. Also no cracks were noted after cyclic thermal loading at 575°C for 1000 hours in 23 hour periods. The tests are being continued to obtain 5000 test hours at temperature. The micro-hardness of the too region is in the range of 240 - 252 Hym. Isolated cases had micro-hardness up to 350 Hym in the zone close to the toe edge for the welding metal VZU 60. There are 8 figures and 8 references: 50 Ny-iet-bloc and 3 non-Soviet-bloc. The reference to the English-language publication reads as follows: F.D. Richardson, Journal of the Iron and Steel Inst. IX, 1953, 33 - 51.

ASSOCIATION: Leninovy závody Plzeň (Lenin Works, Pilsen)

Card 5/5

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e _{tt} † g. v	Α. C. O . •				

Seriautomatic arc wolding, p. 295. (Evaratic, Smatislava, Tol. 3, no. 15, Oct. 194, SC: Monthly list of East Suropean Accessions (EEAL), LC Vol 4, No. 6, June 1945, Uncl



PILOUS, V.

Cold pressure welding of aluminum and copper. p. 204. STR NIRENSTVI Vol 5, no. 3, Mar. 1955 Czechoslovakia

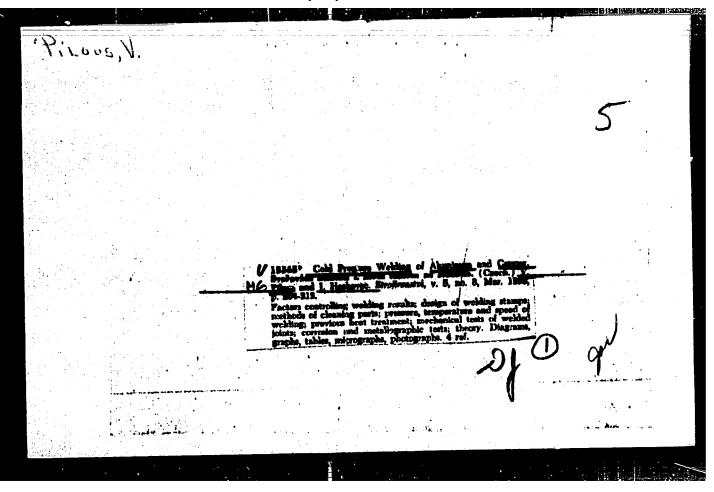
SOURCE: EEAL, Vol 5, no. 7, July 1956

PILOUS, V.

Aluminum and copper cold-pressure butt welding. p. 357.

ZVARANIE, Vol. 4, No. 12, Dec. 1955. Czechoslovakia.

SOUPCF: East European Accessions List, Library of Congress Vol. 5, No. 7, July 1956.



PILOUS, V.

"One Exhanst in Arc Welding." p. 169, Praha, Vol. 2, no. 4, 1954.

SO: East European Accessions List, Vol. 3, No. 9, September 1954, Lib. of Congress

CZECH/14 164 10 13/15 Václav Pilous (Cand Tech. Sci., Engineer) 18.1150 Contribution on the Metaliurgical Weldability of 187200 5% Cr Steels Innoculated with Molybdenum or Tungsten AUTHOR: PERIODICAL: Hutnické Listy, 1959, Nr 10, pp 895.898 ABSTRACT: "Rena" steel with "% Cr innoculated with 0 % molyodenum TITLE: "Rena" steel with 7% or innothiated with 0 % monyodenim is being supplied in the 'as cast' state and also is being supplied in the 'as cast' state and also is being supplied in the Works "K Gottwald", for shaped by the Vitkovice Iron Works being used for shaped by the Vitkovice Iron Works to 600 of and wall high temperature use temperatures up to 600 of and wall media with outflowing temperatures up to save molyidenim temperatures up to 5/5 of In order to save molyidenim temperatures up to 5/5 of In order to save molyidenim and nickel ZVII. Pilson tevaloned a 5% outromium steel and nickel. ZVIL Pilsen, leveloped a 5% chromium steel grade 1555W (CSN -2 2900) in which the star e molybdenum is substituted by icubie the quantity of tunesten (1%) For welding these steels, the Welding Research Institute in Bratislava is applying ferritic perlitic electrodes With a composition similar to that of the welded material with alloying elements in the elect. ode coatings The electrode plant of the Vitkovice Iron Works have produced for this purpose sultable electrodes in which the allcying material is located in the core of the electrode. In this baser the welding properties of 'Mo-W') Card 1/3

CZECH/34-59-10-13/25 Contribution on the Metallurgical Weldability of 5% Cr Steels Innoculated with Molybdenum or Tungsten

> steel are discussed. The weldability of these steels was judged from the hariness characteristic of Jominy rods querched at the faces and from the location of the perlitic front on the isothermal diagrams. The chemical compositions of the materials produced in the experimental heats are given in Table 1, p 895 The test results have confirmed that tungsten increases the stability of the austenite in the ferritin-perlitic range in steels containing 5% chromium. 5% Cr W (1555W and CSN 42 2900) steel in which molybdenum is substituted by double the quantity of tungster (1% W) will have a similar welding behaviour to that of 5% Ct Mo steel (1555 - CSN 17 102). This was proved by the results of cooling experiments at tepped cooling speeds between 450000 and 30 % per hour, sominy end hardening tests and calculations of the coling speeds from isothermal diagrams. By omparing the recing speeds at which a 20% austenite de empesition takes place in the perlitic mose region with speeds readed in the case of welding with pre-heating to a remperature of 300,400 CC

Card 2/3

CZECH,/34 F9-10-13/25

Contribution on the Metallurgical Weldability of 5% Or Steels Innoculated with Molybdenum or Tungsten

and in the case of welding without pre-heating (Table in) it can be seen that in no case will the speeds be so high that the perlits mose of the S curves would be affected. From the point of view of welding, W has a favourable effect on bromium leets since it reduces the stability of the austenite on the region of the bainitio transformation by shifting the nose of the bainitic transformation to the left, thus accelerating the austenite transformation (Figs 6.8). Even if very Even if very thick sheets are welded, the resulting structure in the transient zone of the welled material will be bainite. which is transformed to a surbitive structure with a night notch impact strength after tempering. Welding is usually followed by tempering at 770 °C and cooling in al: There are a figures, 5 tables and 5 references, of which . are English and 1 is German 3 are Czech.

Card

ASSOCIATION:

Výzkomný a zkosební ustav ZVIL. Plzeh

(Research and Test Institute ZVIL, Pilsen

SUBMITTED:

April 15 1/4

2/034/61/000/003/004/011 E073/E335

Pawera, Karel, Engineer, Filous, Václav, Candidate AUTHORS:

of Technical Sciences, Engineer and

Pobořil, František, Engineer Doctor

Microstructure and Mechanical Properties of Weld TITLE:

Joints Between Austenitic and Pearlitic Creepresistant Steels for Boilers Operating at High

Pressures and Temperatures

Hutnické listy, 1961, No. 3, pp. 186 - 197 PERIODICAL:

In thermal power stations with high operating steam temperatures and pressures austenitic steels have to be used TEXT: for the hottest sections of the superheater and the highpressure boiler whilst less thermally stressed sections can be made from cheaper ferritic-pearlitic steels. In 1959 the problem of producing satisfactory weld joints between these two types of steel became acute. Since at the time a satisfactory weld joint between ferritic-pearlitic and austenitic steels was not available, it was decided to verify the possibility of using a welding technology developed in the Card 1/15

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Microstructure and Mechanical ...

Vyzkumny a zkusebný ústav, Závody V. I. Lenina v Flzni (Research and Test Institute of the V.I. Lenin Works, Pilson). In the first part of the paper results published in the literature are reviewed: work is mentioned of A.S. Gel'man and V.S. Popov (Ref. 2), J.T. Tucker, Jr. and F. Eberle (Ref. 3), F. Erdmann-Jernitzer, M. Beckert and H. Schmiedel (Ref. 4), B. Löfblad and E. Lindh (Ref. 5) and H. Linden and H. Henneke (Ref. 6) and information published by the International Nickel Company (Ref. 8) and also work by A.F. Kozajev, A.V. Sibanov (Ref. 9), L. Jenicek (Ref. 10), Z. Eminger, J. Krumpos (Ref. 11) and P. de Marneffe of France (Ref. 13) as well as earlier work of one of the authors (Ref. 1). Practical experience has shown that during heat-treatment and also when the material is held over long periods at the operating temperatures, a decarburised zone, a few tenths of a mm wide, forms in the transient zone in the ferritic-pearlitic steels, whilst in the strip which is directly adjacent to the austenitic weld metal a thin carburised zone forms. This behaviour is attributed to the Card 2/15

Z/034/61/000/003/004/011 E073/E335

Microstructural and Mechanical ...

differing solubility of carbon and the α and γ phases. For weld joints between ferritic-pearlitic and austenitic material which are exposed to high alternating thermal stresses under load, the Lenin (Skoda) Works make the weld using the material VZU 60, which contains 60% Ni and 50% Cr; the coefficient of thermal expansion of this material has a value which is intermediate between that of ferritic-pearlitic and that of austenitic steels (Fig. 3). The solubility of carbon in this material, which contains predominantly Ni, is very low and therefore it forms an effective barrier against carbon diffusion. Compared with similar fabricated electrodes produced by Messrs. Wiggin in Great Britain, the Czech-produced electrodes are cast rods, which are considerably cheaper. The V.I. Lenin Works have developed a reliable process for manufacturing such welded rods; the only scrap is that caused by the gatings, amounting to 25-30% of the charge weight. After casting, the rods are sand-blasted and cold-forged on a rotary forging machine TOS R 16 to a diameter of 3.5 mm. These electrodes are used for argon-arc welding of high-alloy alloys

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Microstructural and Mechanical ...

operating at temperatures up to 700 °C. The welding metal has the most favourable mechanical and physical properties after hardening at 750 °C (250 H_V , impact strength up to 10 mkg/cm2). The hardness of the welding metal after welding is 160 Hy with an impact strength of 9 mkg/cm. The mechanical properties of this metal are given in Table 1. The proneness to temper trittleness was investigated at the temperatures of 600, 650 and 700 °C for 1 000 hours; the impact strength does not change appreciably by the ageing and a drop by about 20% was detected only after cooling to and a drop by about 20% was detected only after cooling to 20°C, which is attributed to the fact that the weld metal was perfectly hardened. The experiments were made on welds joining tubes of a diameter of 32 x 5 mm of the steel CSN 15225 (Lof special extra) with tubes of equal dimensions of the steel CSN 17481 (MnCrTi 17/7). The composition (in %) ČSN 15225 - 0.10-0.15 C, 0.45-0.65 Mn, 0.15-0.25 Si, 0.40-0.50 Cr. 0.90-1.00 Mo, 0.20-0.35 V, max 0.045 P and max. 0.045 S; Card 4/15

Microstructural and Mechanical...

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CSN 17481 - 0.05-0.12 C, 17.0-19.0 Mn, max. 0.70 Si, 7.0-8.0 Cr, 0.30-0.60 Ti, max. 0.040 P and max. 0.035 S. The following combinations of weld joints and heat-treatment were used in the experiments:

Type of weld seam	Base Material	Weld Seam	Heat treatment (after welding)
A	15225/17481	vzú 60	a) 980°C/0.5 h/air 680°C/1 h/air b) 680°C/2 h/air c) without heat treatment
В	15225/15225	VZÜ 60	a) 980°C/0.5 h/air 680°C/1 h/air
С	17481/17481	vzu 60	a) 980°C/0.5 h/air 680°C/1 h/air
Cl	17481/17481	"C"	d)1000°C/0.5 h/air.

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Microstructural and Mechanical...

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The purpose of the combinations B and C was to determine the additional influence of the base materials 15225 and 17481 on the properties of the welding material VZU 60; the purpose of the combination Cl was to evaluate the stability of the weld of the austenitic tubes from the steel 17481 welded by the argon-arc method, using the material "C" (MnCrNo(Nb) 17/7) in accordance with the technology worked out by J. Novotný (Refs.16,17) at the Vyzkumný ústav svářečský (Welding Research Institute). The heat-treatment a) corresponds to that normally specified for the steel CSN 15225; b) to that specified for erection weld seams of the steel CSN 15225; d) corresponds to the heat-treatment specified for welds of the steel ČSN 17481. In contrast to the technology of argon-arc welding of uniform materials, where it is advantageous to fuse the root of the weld without additional material, it is in this case necessary to deposit material from the VZ $\tilde{\mathbf{U}}$ 60 electrode also into the root, so as to prevent diffusion of carbon from the ferritic-pearlitic into the austenitic material. The results of X-ray tests with an oblique beam through two walls did not prove satisfactory

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from the point of view of giving a reliable indication of the quality of the weld seam and should not be used for quality control. Therefore, the authors considered using an X-ray beam in two mutually perpendicular planes. In the bending tests (of A, B, C) bending angles between 38 and 73 were achieved before the first crack occurred and in two cases bending angles of 120 and 135 were achieved without any crack. These results show that the weld joint has a satisfactory plasticity. Bending tests on the tubes welded with the electrodes "C" showed good results; bending angles of 1800 were achieved without fracture. In tensile tests at 180° were achieved without fracture. In tensile tests at 20°C, yield-point values of 30 - 41.4 kg/mm were achieved, with strength values of 45.7 - 59.5 kg/mm and contraction of 10.4 - 14.7%. The fractures always occurred in the weld metal VZÚ 60 which, at this temperature, has a lower strength than both the base materials, the mechanical properties are fully in accordance with the respective values for the cast alloy VZU 60. Tensile tests at 575 °C showed yield-point values of 13.2 - 18.9 kg/mm², strength values of $27.4 - 35.5 \text{kg/mm}^2$ Card 7/15

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Microstructural and Mechanical

and an elongation of 15.3 - 22.7%; fractures almost always occurred in the austenite and the results correspond with the appropriate values for the material ČSN 17481 at that temperature. The results of metallographic tests confirm that the alloy VZU 60 is suitable for welding ferritic-pearlitic steels with austenitic steels; the coefficient of thermal expansion of this alloy has a value which is intermediate between the respective values of the two materials. Due to its high nickel content, diffusion of carbon from the ferriticpearlitic into the austenitic steel is prevented. The results of creep-rupture tests for specimens of the dimensions as shown in Fig. 13 (tube diameter 32 x 5 mm) are plotted in Fig. 14. It can be seen that the results roughly correspond to a straight line representing average values for the material 15225. The method of heat-treatment of the joints had practically no influence on the results. The fractures always occurred in the transition zone of the base material 15225. Compared with the respective values currently assumed for these materials, the strength under creep conditions of the Card 8/15

Microstructural and Mechanical

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transient zone of the material 15225 was somewhat lower and that of the material 17481 was somewhat higher. In 3-month corrosion tests the corrosion speed of both base materials was about 0.7 - 1.7 g/m²day corresponding approximately to 0.03 - 0.09 mm/year. In no case was an intensive or local

corrosion attack detected in the weld, neither the material "C" nor the material VZÜ 60 showed signs of having been attacked by corrosion in a power-station condensate which was saturated at 20 °C with oxygen and carbon dioxide. Acknowledgments are expressed to Duchek (VZÜ-ZVIL) and Pajürka (VŽKG), who made the experimental weld joints Engineer Toman and Engineer Sedenko (VZKG) and Tykal (VÜHZ), who carried out the metallographic analyses Baier (VŽKG) and Franc (VÜHŽ), for carrying out the mechanical and creep tests Engineer Svefe; (SVÜOM) for carrying out the corrosion tests and also to Engineer Huber (VŽKG). There are 14 figures, 7 tables and 20 references. 6 Czech and 14 non-Czech.

Card 9/15

2/034/61/000/003/004/011 Microstructural and Mechanical LU73/E335

ASSOCIATIONS

VŽKG Ostrava (K. Pawera) VŽŰ ZVIL Pilsen (V. Pilous) VUHZ Prague (F. Pobořil)

SUBMITTED: November 14 1960

Card 10/15

Microstructural	and Methanical

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Tempera- ture. C	Heat Treat- ment	Yield point kg/mm ²	strength	Elong- ation (5d),	Contra- ction %	Impact Strength, mkg/cm ²
20	No heat- treat- ment	23,2	4,4,4	25	25	9
20	۰	33,4	55.6	20	20	7
500	4	17.2	34,4	26	28	9
550		16.5	32.4	27	28	ģ
600	.)	15.5	30.2	27	28	ģ
650	8 1	14.5	29.6	24	27	9
700	1 3	13.2	28 4	22	26	9

Card 11/15

Z/034/61/000/003/004/011 Microstructural and Fechanical . E073/E335

Table 2.

Composition of high-frequency heat No 479 0 05 0 21 0.47 0.009 0 025 1805 0 15 1, 22 10.94 2.10 2.19 0.47

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Microstructural and Mechanical ...

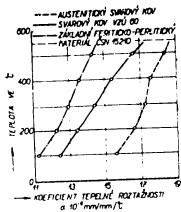
Fig. 3: Coefficient of thermal expansion of austenitic electrode material E 391, the weld alloy VZÚ 60 and of the base ferrite-pearlite material CSN 15210 in the temperature range 100 to 550 °C.

Temperature, OC versus coefficient of thermal expansion,

 $\alpha \times 10^{-6} \text{ mm/mm/}^{\circ}\text{C}$.

--- Aus:enitic weld metal Welding alloy VZÚ 60

Base ferrite-pearlite
Laterial CSN 15210

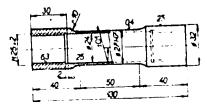


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Microstructural and Mechanical ...

Fig. 13: Test specimen from the tube of diameter 32 x 5 mm for creep-rupture tests.



Obr. 13. Zkušebni vzorek z trubky Ø 32×5 mm pro zkoušku tečení do lomu.

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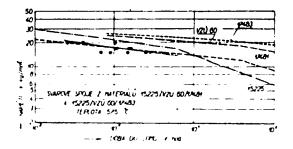
Fig. 14:

Microstructural and Mechanical ...

Results of creep-rupture tests of experimental weld joints.

Stress, kg/mm versus time-to-failure, hours.

Weld joints from the materials 15225/VZU 60/17481 and 15225/VZU 60/17483
Temperature 575 °C.



Card 15/15

The state of the s

Monthly list of East European Accessions (EFAI), LC, Vol. F, No. 6, August 1959.
Uncla.

PILOTS, V.

Contribution to the properties of 5 391 and 5 '91 austematic electrodes. P. . /.

ZVARANTE. (Ministersive hitreho promysla a midnych tani a Ministersive sin i persiva. Fratislava, Dzechoslovakia. Vol. M., no. 7, July 1969.

Monthly list of East European Accessions (EMAI) 17, Vol. M. no. 15, et. 1905. Incl.

67013 18.1150 CZECH/34-54 10-13/25 18 7200 Václav Pilous (Cand Tech Sci., Engineer) AUTHOR: Contribution on the Metallurgical Weldability of 5% Cr Steels, Innoculated with Molybdenum or Tungsten TITLE: PERIODICAL: Hutnické Listy, 1959, Nr 10, pp 805-898 ABSTRACT: "Rena" steel with 5% Cr innoculated with 0.5% molyodenum is being supplied in the 'as cast' state and also shaped by the Vitkovice Iron Works "K Gottwald", for high temperature use. This steel is being used for media with outflowing temperatures up to 600 oC and wall temperatures up to 575 of In order to save molybdenum and nickel, ZVIL. Pilsen, developed a 5% chromium steel grade 1555W (CSN 42 2900) in which the scarce molyodenum is substituted by double the quantity of tungsten (1%). For welding these steels, the Welding Research Institute in Bratislava is applying ferritic perlitic electrodes with a composition similar to that of the welded material with alloying elements in the electrode coatings The electrode plant of the Vitkovice Iron Works have produced for this purpose suitable electrodes in which the alloying material is located in the core of the Card

1/3

APPROVED FOR RELEASE: 06/15/2000 CIA-RDP86-00513R001340910005-8"

electrode. In this paper the welding properties of (Mo-W)

67013

Contribution on the Metallurgical Weldability of 5% Cr Steels

steel are discussed. steels was judged from the hardness characteristic of Jominy rods quenched at the faces and from the location of the perlitic front on the isothermal diagrams. The chemical compositions of the materials produced in the experimental heats are given in Table 1, p 895. The test results have confirmed that tungsten increases the stability of the austenite in the ferritic-perlitic range in steels containing 5% chromium. 5% Cr W (1555W and CSN 42 2900) steel in which molybdenum is substituted by double the quantity of tungsten (1% W) will have a similar welding behaviour to that of 5% Cr Mo steel (1555 - CSN 17 102). This was proved by the results of cooling experiments at stepped cooling speeds between 450000 and 20 oc per hour, Jominy end hardening tests and calculations of the cooling speeds from isothermal diagrams. By comparing the cooling speeds at which a 20% austenite decomposition takes place in the perlitic nose region with speeds reached in the case of -Welding with pre-heating to a temperature of 300-400 C

Card 2/3

67013

CZECH/34.59-10-13/25

Contribution on the Metallurgical Weldability of 5% Cr Steels

Innoculated with Molybdenum of Tungsten

and in the case of welding without pre-heating (fable it can be seen that in no case will the speeds be so high that the perlitte nose of the S curves would be affected From the point of view of welding. W has a favourable effe t on bromium steels since it reduces the stability of the austenite in the region of the bainitic transformation by shifting the nose of the bainitic transformation to the left, thus accelerating the austenite transformation (Figs 6.8) Even if very thick sheets are welded, the resulting structure in the transient zone of the welded material will be bainitiwhich is transformed to a sorbitic structure with a high notch impact strength after tempering. Welding is usually followed by tempering at 720 oc and cooling in air. There are 9 figures. 5 tables and h references, of which 3 are Czech,

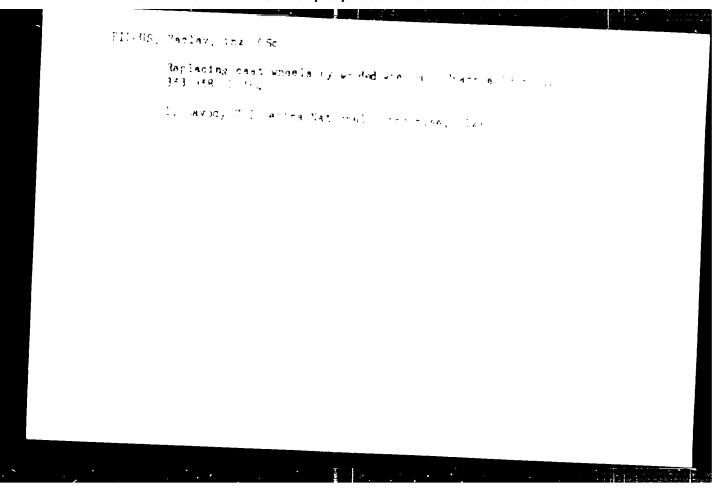
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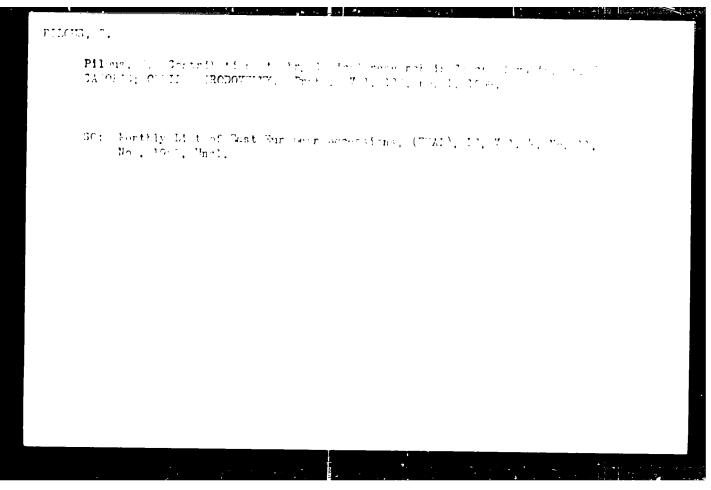
Výzkumný a zmisební ústav ZVIL, Plzeh ASSOCIATION:

(Research and Test Institute ZVIL, Pilsen

SUBMITTED:

April 18, 1959





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The moss Pseudolaskea Saviana Latzel in Slovakia. F. . . .

SIOLOGIA. (Slovenska akademia clei) Bratis ava CZECIKULU.ALIA

Vol. 10, ho. 4, 1955.

SUR E: East European Accessions List (EEAL) Library

of Congress, Vol. 5, No. 1, January, 1950

Diseases of mossess (Bryephyta) and ferns (Pteridophyta), which are considered or suspected of being of virus origin. Chekh biol. 2 no.2:84-92 ap '53. (MIRA 7:2)

1. Institut biologii ChōaN, fitopatologiya, Praha. (Mosses--Diseases and pests) (Ferns--Diseases and pests) (Virus diseases of plants)

Filcus, 2.	
BLATTNY, C.; PILOUS, Z. "Diseases of Mosses (Bryophyta) and Ferns (Pteridop are Considered or Suspected to be of Virus Origin." p. 84. (Chekhoslovatsk Vol. 2, no. 2, Apr. 1953. Praha).	hyta) which aia Biologiia.
East European Vol. 3, No.6 SO: Monthly List of Accessions Library of Congress, June	1950, Uncl.

BRANDIS, S.A.; IOSEL'SON, S.A.; PILDVITSKAYA, V.N..

Functional changes in the body at rest and at work during prolonged

inhatation of gas mixtures containing large amounts of oxygen.

Fiziol. Zhur. 46 no. 7:801-809 Jl '60. (MIRA 13:8)

1. From the Central Research Laboratory for the Mining Salvation Work, Stalino, Donbass.
(OXYGEN—PHYSIOLOGICAL EFFECT) (EXERCISE)

The state of the formattic state of the stat

KOGAH, D.A., professor; PILOVITSKAYA, V.N., mladshiy nauchnyy sotrudnik;

SAYAPIKA, L.I.

Antitoxic hepstic function in fractures of the long bones as affected by some physical factors. Ortop., travm. i protes. 17 no.3:68 My-Je '56 (MIRA 9:12)

1. Is Usbekskogo nauchmo-issledovatel'skogo institute ortopedii, travmatologii i protexirovaniya (dir. - kandidat meditsinskikh nauk A.Sh.Shakirov)

(LIVER) (FRACTURES) (PHYSICAL THERAPY)

BRANDIS, S.A.; PILOVITSKAYA, V.N.

Functional changes in the body at rest and during work after breathing for many hours a gas mixture containing a high concentration of oxygen and a small concentration of carbon dioxide. Fiziol. zhur. 48 no.4:455-463 Ap '62. (MIDA 15:6

1. From the Central Research Laboratory for Mining Rescue,
Donetz Regional Economic Council, Donetz.

(RESPIRATION)

(STRESS (PHYSIOLOGY))

(METABOLISM, DISORDERS OF)

MANVELYAN, M.G.; NADZHARYAN, A.K.; AKOPYAN, Z.A.; PILOYAN, E.G.; GAMBARYAN, S.G.; BABAYAN, S.A.

Changes of nepheline syenite and minerals constituting it during their treatment by potassium hydroxide solutions.

Izv. AN Arm. SSR. Khim.nauki 14:417-423 '61. (MIRA 15:1)

1. Institut khimii Sovnarkhoza Armyanskoy SSR. (Nepheline syenite)

PILOYAN, G.

Minerals genetically associated with the ultrabasic (magnesia-silicate) rocks of the northeastern shores of Lake Sevan.

Prom.Arm. 4 no.12:8-13 D '61. (MIRA 15:2)

1. Nachal nik Sevanskoy geologorazvedochnoy partii. (Lake Sevan Region—Minerals)

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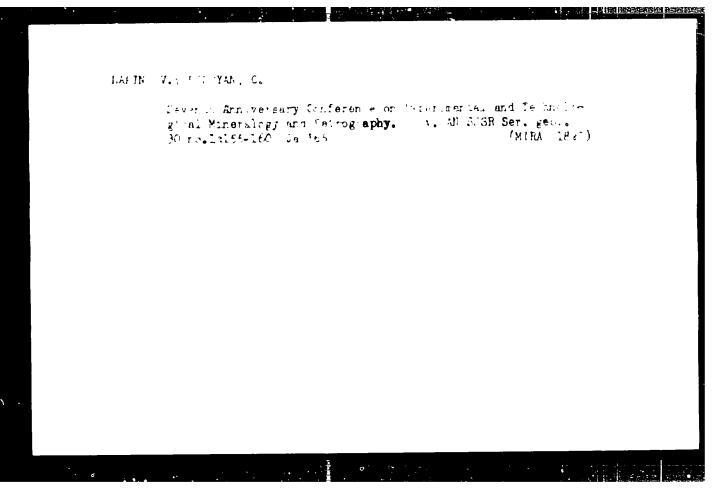
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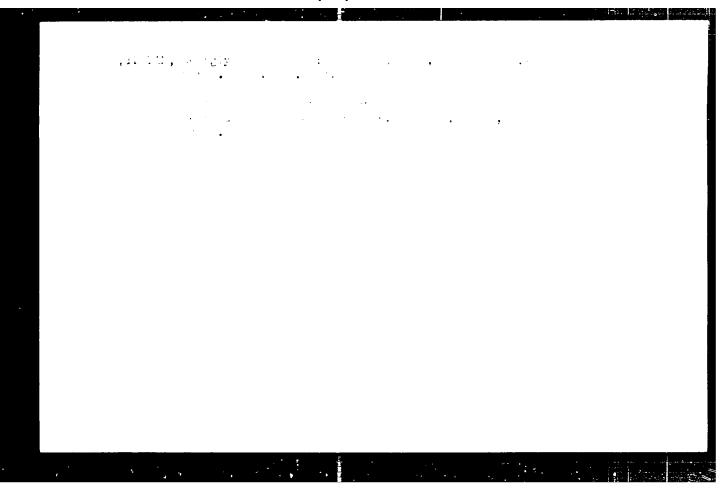
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